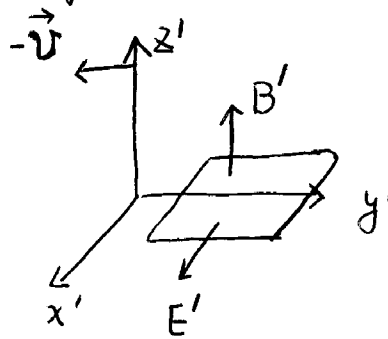
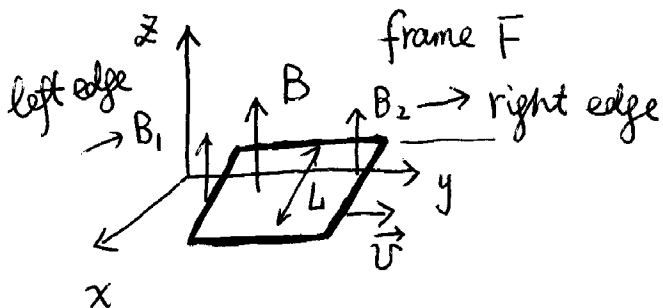


# Lect 5: Electro-magnetic induction

①

§ a loop of wire moving in non-uniform B-field



lab frame with zero E field.

Two edges (left and right) will feel Lorentz force, <sup>for</sup> and the other edges, along the loop

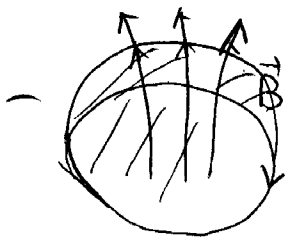
the Lorentz force is perpendicular to the loop.

$$\oint \vec{f} \cdot d\vec{s} = \frac{qv}{c} (B_1 - B_2) L \quad \text{define emf: } \mathcal{E} = \frac{\oint \vec{f} \cdot d\vec{s}}{q} = \frac{Lv}{c} (B_1 - B_2)$$

or we define magnetic flux  $\Phi = \iint d\vec{a} \cdot \vec{B}$

$$\frac{d\Phi}{dt} = \frac{B_2 L v \Delta t - B_1 L v \Delta t}{\Delta t} = (B_2 - B_1) Lv \Rightarrow \boxed{\mathcal{E} = -\frac{1}{c} \frac{d\Phi}{dt}}$$

due to the fact that there's no magnetic charge  $\nabla \cdot \vec{B} = 0$ , the flux penetrating a surface only depends on the boundary. As long as the boundary is specified, it doesn't matter which surfaces you measure.



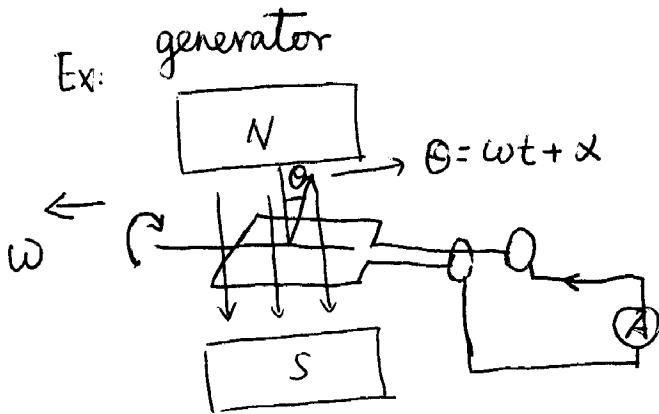
$\mathcal{E}$  can also be represented as

$$\mathcal{E} = \frac{1}{c} \oint (\vec{v} \times \vec{B}) \cdot d\vec{\ell}$$

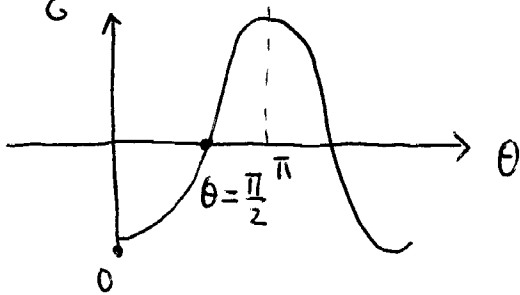
$$\mathcal{E} = -\frac{1}{c} \frac{d\Phi}{dt} \quad \leftarrow \text{Lentz's law,}$$

②

the flux generated by the induced current should be in an opposite direction to the change of  $\Phi$ , (not  $\Phi$  itself, but  $d\Phi$ !)



$$\Phi = S \cdot B \sin(\omega t + \alpha) \Rightarrow \mathcal{E} = -\frac{1}{c} \frac{d\Phi}{dt} = -\frac{SB\omega}{c} \cos(\omega t + \alpha)$$



$\S$ : a stationary loop in a changing B-field

In the comoving frame, there exists electric field  $\vec{E}'$ . The emf is purely generated by  $E'$ .

$$\vec{E}' = -\frac{\vec{v}' \times \vec{B}'}{c} = \frac{\vec{v} \times \vec{B}'}{c}$$

$$\oint \vec{E}' \cdot d\vec{s}' = \frac{L v}{c} (\vec{B}'_1 - \vec{B}'_2) \quad \text{again} \quad \mathcal{E}' = -\frac{1}{c} \frac{d\Phi'}{dt'}$$

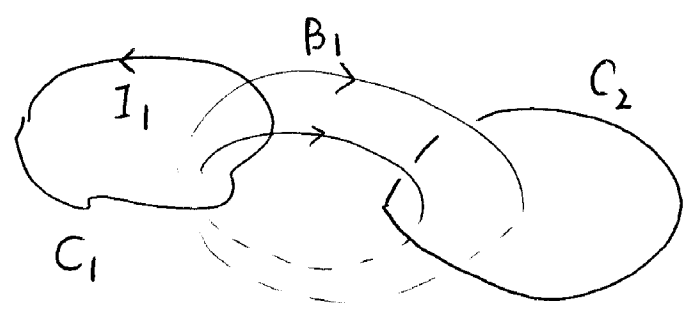
please note that we need to use  $\mathcal{E}'$ ,  $B'$  and  $t'$  consistently.

$$\Rightarrow \text{Faraday's law} \quad \oint \vec{E} \cdot d\vec{s} = -\frac{1}{c} \frac{d}{dt} \iint \vec{B} \cdot d\vec{a}$$

$$\Leftrightarrow \nabla \times \vec{E} = -\frac{1}{c} \frac{\partial \vec{B}}{\partial t}$$

§ mutual conductance

Consider two current loops  $C_1$  and  $C_2$  (position fixed,



flux from  $I_1$  through loop  $C_2$

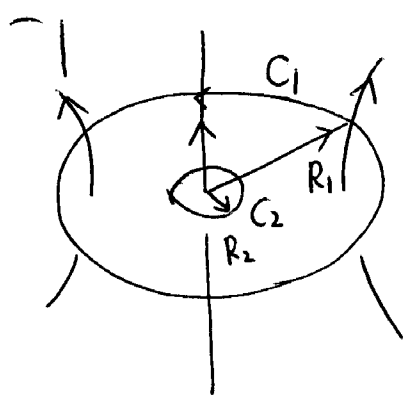
$$\Phi_{21} = \iint_{S_2} \vec{B} \cdot d\vec{a}_2 \propto I_1 \cdot \text{const}$$

$$\Rightarrow \mathcal{E}_{21} = - \frac{\text{const}}{c} \frac{dI_1}{dt} = -M_{21} \frac{dI_1}{dt}$$

Similarly we can calculate the emf in loop 1, generated by the current change of  $C_2$ .

$$\mathcal{E}_{12} = -M_{12} \frac{dI_2}{dt}$$

Ex:  $B_1$  at the center of the ring



$$B_1 = \frac{2\pi I_1}{c R_1}, \quad \Phi_{21} = \pi R_2^2 \frac{2\pi I_1}{c R_1} = \frac{2\pi^2 I_1 R_2^2}{c R_1}$$

$$\Rightarrow \mathcal{E}_1 = - \frac{2\pi^2 R_2^2}{c^2 R_1} \frac{dI_1}{dt}, \quad \boxed{M_{21} = \frac{2\pi^2 R_2^2}{c^2 R_1}}$$

$$[M] = \text{Henry} = \frac{[\text{Volt}]}{[\text{Amp}]/[\text{CS}]}$$

parameters of  $R_1, R_2$  are not symmetric

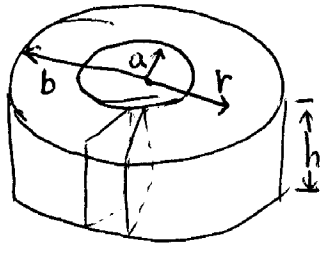
reciprocal theorem:  $\boxed{M_{21} = M_{12}}$ , why?

$$\begin{aligned} \Phi_{21} &= \oint_{C_2} \vec{A}_{21}(\vec{r}_2) \cdot d\vec{l}_2 \\ \vec{A}_{21}(\vec{r}_2) &= \oint_{C_1} \frac{I_1(\vec{r}_1) d\vec{l}_1}{r_{21}} \end{aligned} \quad \Rightarrow \quad \begin{aligned} \Phi_{21} &= \frac{I_1}{c} \oint_{C_2} \oint_{C_1} \frac{d\vec{l}_2 \cdot d\vec{l}_1}{r_{21}} \\ M_{21} &= \frac{1}{c} \oint_{C_2} \oint_{C_1} \frac{d\vec{l}_2 \cdot d\vec{l}_1}{r_{21}} = M_{12} \end{aligned}$$

§ Self-inductance — the emf in loop  $C_1$  generated by the change of current  $I_1$

$$\mathcal{E}_{11} = -\frac{1}{c} \frac{d\Phi_{11}}{dt}$$

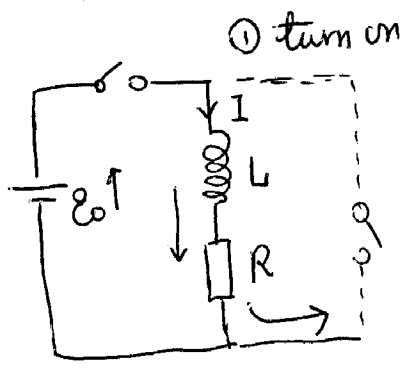
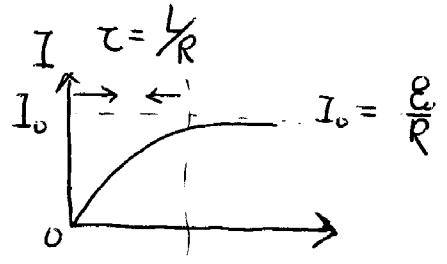
$$= -L_1 \frac{dI_1}{dt}$$



$$\Rightarrow B \cdot 2\pi r = \frac{4\pi}{c} NI \Rightarrow B = \frac{2NI}{cr}$$

$$\Phi = \int_a^b \frac{2NI}{cr} h \, dr = \frac{2NIh}{c} \ln\left(\frac{b}{a}\right) \Rightarrow L = \frac{2N^2 h}{c^2} \ln\left(\frac{b}{a}\right)$$

§ circuit contains  $R$  and  $L$



$$u = IR = \mathcal{E}_0 - L \frac{dI}{dt}$$

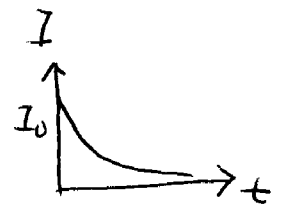
$$\text{or } \begin{cases} \frac{dI}{dt} = -\frac{R}{L} I + \frac{\mathcal{E}_0}{L} = -\frac{R}{L} \left( I - \frac{\mathcal{E}_0}{R} \right) \\ I(0) = 0 \end{cases}$$

$$\Rightarrow I - \frac{\mathcal{E}_0}{R} = -\frac{\mathcal{E}_0}{R} e^{-\frac{R}{L}t} \Rightarrow I = \frac{\mathcal{E}_0}{R} (1 - e^{-\frac{R}{L}t})$$

$L$  prevent the jump of current.

② turn off

$$-L \frac{dI}{dt} = RI \Rightarrow I = I_0 e^{-\frac{R}{L}t}$$



§ Energy stored in magnetic field

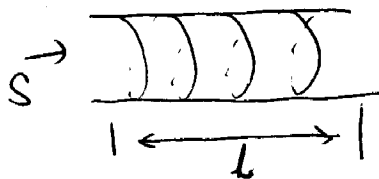
The energy dissipation on  $R$

$$U = R \int_0^{+\infty} I^2(t) dt = R I_0^2 \int_0^{+\infty} e^{-\frac{2R}{L}t} dt = R I_0^2 \cdot \frac{L}{2R} = \frac{L I_0^2}{2}$$

This amount of energy was originally stored in the coil as magnetic energy (5)

energy 
$$U = \frac{1}{2} LI^2$$

Consider a long coil



$$\Phi = NSB = NSB$$

$$B = \frac{4\pi}{c} \frac{NI}{l}$$

$$\Rightarrow \Phi = \frac{4\pi}{c} \frac{N^2 SI}{l}$$

$$\Rightarrow U = \frac{1}{2} \frac{4\pi}{c} \frac{N^2 S}{l} I^2$$

$$= \left( \frac{4\pi}{c} \frac{NI}{l} \right)^2 \frac{S \cdot l}{8\pi} = \frac{B^2 \cdot \text{Vol}}{8\pi}$$

$$\Rightarrow L = \frac{4\pi}{c} \frac{N^2 S}{l}$$

$$\Rightarrow \text{energy (magnetic) density} = \frac{B^2}{8\pi}$$

c.f. electric energy density  $\frac{E^2}{8\pi}$

generalize to non-uniform E and B field

$$U = \frac{1}{8\pi} \int (E^2 + B^2) dv$$

# Lect 6. Displacement current

what's left?

$$\nabla \cdot \vec{E} = 4\pi\rho$$

Gauss's law

$$\nabla \cdot (\nabla \times \vec{B}) = \frac{4\pi}{c} \nabla \cdot \vec{j} \neq 0$$

$$\nabla \times \vec{E} = -\frac{1}{c} \frac{\partial \vec{B}}{\partial t}$$

Faraday's law

$$\nabla \cdot \vec{B} = 0$$

no magnetic monopole

$$\nabla \times \vec{B} = \frac{4\pi}{c} (\vec{j} + \vec{j}_D)$$

$$\nabla \times \vec{B} = \frac{4\pi}{c} \vec{j}$$

Ampere's law

$$\nabla \cdot \vec{j} + \frac{\partial \rho}{\partial t} = 0$$

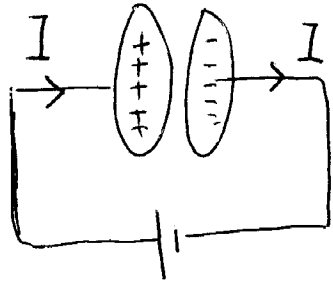
continuity equation

$$\nabla \cdot (\vec{j} + \vec{j}_D) = 0 \Rightarrow \nabla \cdot \vec{j}_D = + \frac{\partial \rho}{\partial t} = + \frac{1}{4\pi} \nabla \cdot \vec{E} \leftarrow \text{Choose } \vec{j}_D = \frac{1}{4\pi} \frac{\partial \vec{E}}{\partial t}$$

$$\Rightarrow \boxed{\nabla \times \vec{B} = \frac{4\pi}{c} \vec{j} + \frac{1}{c} \frac{\partial \vec{E}}{\partial t}}$$

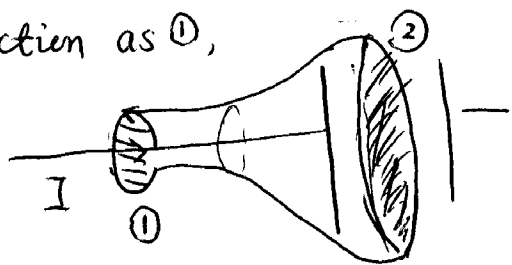
Maxwell's contribution

Suppose we provide a steady charge current to a capacitor.



we know  $\oint \vec{B} \cdot d\vec{l} = \frac{4\pi}{c} I$  if I choose

the cross section as ①,



I can also choose the cross section as ②,

there are no I.  $\oint \vec{B} \cdot d\vec{l} = 0$  ? No! We can pretend that

current is continuous, but this time it's relate by  $\vec{j}_D = \frac{1}{4\pi} \frac{\partial \vec{E}}{\partial t}$

$$\text{we can show that } E = 4\pi\sigma \Rightarrow \vec{j}_D = \frac{1}{4\pi} \frac{\partial E}{\partial t} = \frac{\partial \sigma}{\partial t} = \frac{I}{S} = \vec{j}$$

②  
 { E & M waves

In the region without charge and current, Maxwell equations reduces to

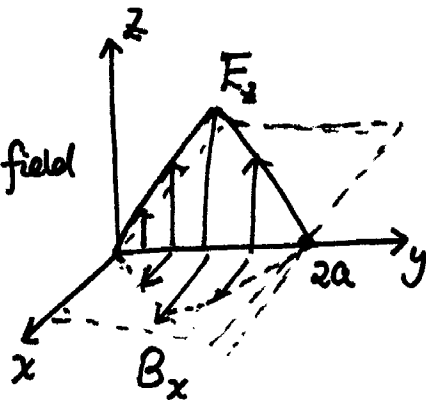
$$\begin{cases} \nabla \times \vec{E} = -\frac{1}{c} \frac{\partial \vec{B}}{\partial t} & , \quad \nabla \cdot \vec{E} = 0 \\ \nabla \times \vec{B} = \frac{1}{c} \frac{\partial \vec{E}}{\partial t} & , \quad \nabla \cdot \vec{B} = 0 \end{cases}$$

E. M field can propagate in the free space without source. It does not

need a media like sound wave.  $\vec{E}, \vec{B}$  do not need an underlying material field like in the elasticity theory.

Consider at  $t=0$ , in the region between  $y=0$  and  $2a$ , we have the following  $\vec{E}, \vec{B}$  field

$$(t=0) \begin{cases} E_z = E_0 \frac{y}{a} & , \quad (0 \leq y \leq a) \\ E_z = E_0 \left( \frac{2a-y}{a} \right) & , \quad (a \leq y \leq 2a) \\ B_x = B_0 \frac{y}{a} & \quad (0 \leq y \leq a) \\ B_x = B_0 \left( \frac{2a-y}{a} \right) & (a \leq y \leq 2a) \end{cases}$$



they satisfy  $\vec{B} = \hat{y} \times \vec{E}$

We can make it propagates by plugging in  $y \rightarrow y-ct$ , i.e.

$$\begin{cases} E_z = E_0 \frac{y-ct}{a} & 0 \leq y-ct \leq a \\ E_z = E_0 \frac{2a-(y-ct)}{a} & a \leq y-ct \leq 2a \end{cases} \quad \text{and} \quad \begin{cases} B_x = B_0 \frac{y-ct}{a} & 0 \leq y-ct \leq a \\ B_x = B_0 \left( \frac{2a-(y-ct)}{a} \right) & a \leq y-ct \leq 2a \end{cases}$$

Check in the region  $0 \leq y-ct \leq a$

$$\nabla \times \vec{E} = \hat{x} \frac{\partial E_z}{\partial y} = \frac{E_0}{a} \hat{x} \quad , \quad \nabla \times \vec{B} = -\hat{z} \frac{\partial B_x}{\partial y} = -\frac{B_0}{a} \hat{z}$$

$$\nabla \cdot \vec{E} = 0$$

$$\nabla \cdot \vec{B} = 0$$

in the region  $a \leq y-ct \leq 2a$

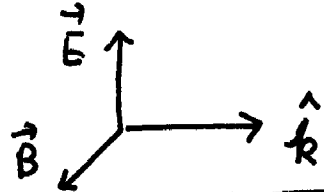
$$\nabla \times \vec{E} = -\frac{E_0}{a} \hat{x}, \quad \nabla \times \vec{B} = \frac{B_0}{a} \hat{z}$$

Similarly, in the region  $0 \leq y-ct \leq a$  and  $a \leq y-ct \leq 2a$

$$\frac{\partial E}{\partial t} = -\frac{c}{a} E_0 \hat{z}, \quad \frac{\partial B}{\partial t} = -\frac{c}{a} B_0 \hat{x}; \quad \frac{\partial E}{\partial t} = \frac{c}{a} E_0 \hat{z}, \quad \frac{\partial B}{\partial t} = \frac{c}{a} B_0 \hat{x}$$

$$\Rightarrow \text{they satisfy } \nabla \times \vec{E} = -\frac{1}{c} \frac{\partial \vec{B}}{\partial t}, \text{ and } \nabla \times \vec{B} = \frac{1}{c} \frac{\partial \vec{E}}{\partial t}.$$

§ In general: for a  $\vec{E}, \vec{B}$  configuration and propagation direction  $\hat{k}$



form a triad, with  $\vec{B}(\vec{r} \cdot \hat{k} - ct) = \hat{k} \times \vec{E}(\vec{r} \cdot \hat{k} - ct)$ ,

it satisfies Maxwell equation.

$$\begin{aligned} \nabla \times \vec{B} &= \nabla \times (\hat{k} \times \vec{E}(\vec{r} \cdot \hat{k} - ct)) = \hat{k} (\nabla \cdot \vec{E}) - (\hat{k} \cdot \nabla) \vec{E} \\ &= -(\hat{k} \cdot \nabla) \vec{E} = -\frac{1}{c} \frac{\partial \vec{E}}{\partial t} \end{aligned}$$

$$\nabla \times \vec{E} = \nabla \times (-\hat{k} \times \vec{B}(\vec{r} \cdot \hat{k} - ct)) = -\hat{k} (\nabla \cdot \vec{B}) + (\hat{k} \cdot \nabla) \vec{B} = \frac{1}{c} \frac{\partial \vec{B}}{\partial t}$$

From Lorentz transformation of  $\vec{E}, \vec{B}$  field, we can check

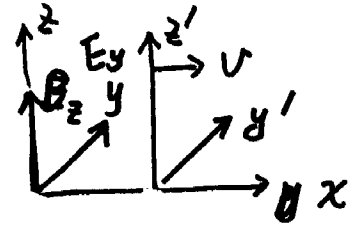
$$E^2 - B^2 \quad \text{and} \quad \vec{E} \cdot \vec{B} \quad \text{are invariant.}$$

$$\Rightarrow |E| = |B| \quad \text{and} \quad \vec{E} \perp \vec{B} \quad \text{cannot change.}$$



light velocity is always "c" in any frame.

suppose in the frame F, the  $\vec{E}, \vec{B}$  fields satisfy



$$\begin{cases} \vec{B} = f(x-ct) \hat{z} \\ \vec{E} = f(x-ct) \hat{y} \end{cases}$$

In the frame  $F'$ , in which  $E', B'$  transforms

$$B'_z(x', t') = \gamma (B_z(x, t) - \beta E_y(x, t)) = \gamma (1 - \beta) f(x - ct)$$

$$E'_y(x', t') = \gamma (E_y(x, t) - \beta B_z(x, t)) = \gamma (1 - \beta) f(x - ct)$$

$$x = \gamma x' - \gamma \beta c t'$$

$$c t = -\gamma \beta x' + \gamma c t' \Rightarrow x - ct = \gamma (1 + \beta) (x' - c t')$$

$$\Rightarrow \begin{cases} B'_z(x', t') = \gamma (1 - \beta) f(\gamma (1 + \beta) (x' - c t')) = \gamma (1 - \beta) f'(x' - c t') \\ E'_y(x', t') = \gamma (1 - \beta) f(\gamma (1 + \beta) (x' - c t')) = \gamma (1 - \beta) f'(x' - c t') \end{cases}$$

$\Rightarrow B'_z, E'_y$  satisfy the Maxwell equation

$$\nabla' \times \vec{B}' = \frac{1}{c} \frac{\partial \vec{E}'}{\partial t'}, \quad \nabla' \times \vec{E}' = -\frac{1}{c} \frac{\partial \vec{B}'}{\partial t'}$$